

# Research Projects in Electronic Engineering at UPC Track – Industrial Electronics

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Sala de Conferències ETSEIAT

## Hybrid Modulators for conducted EMI suppression in modular-parallel topology

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d'Enginyeria  
Electrònica

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6. **Conclusions**

# 1.- Introduction

The present trend in Power Electronics to improve performance is

## SYSTEM INTEGRATION

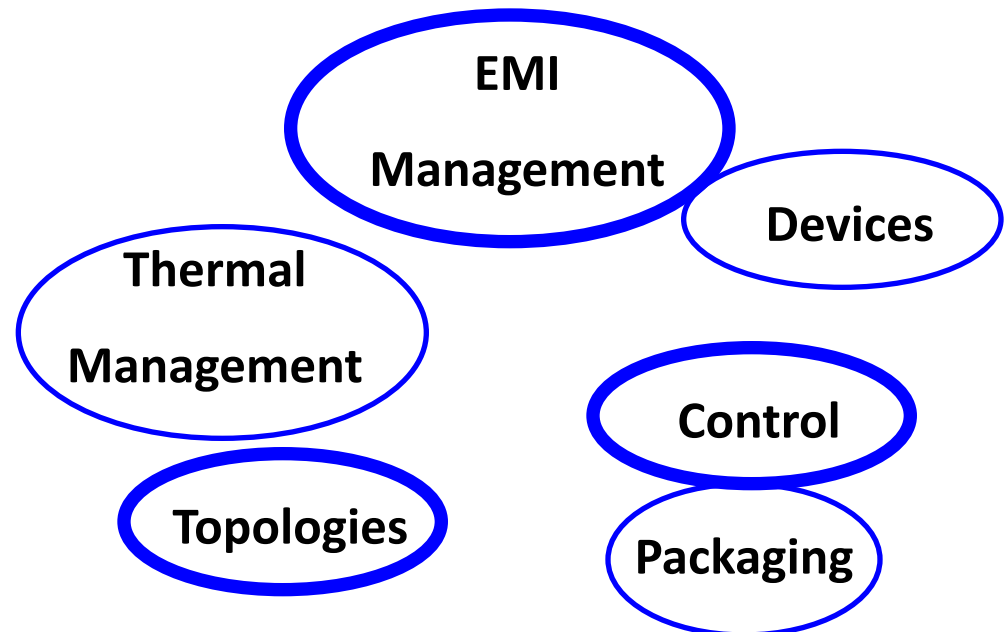
Power density [kW/dm<sup>3</sup>]

Power per unit weight [kW/kg]

Relative cost [€/kW]

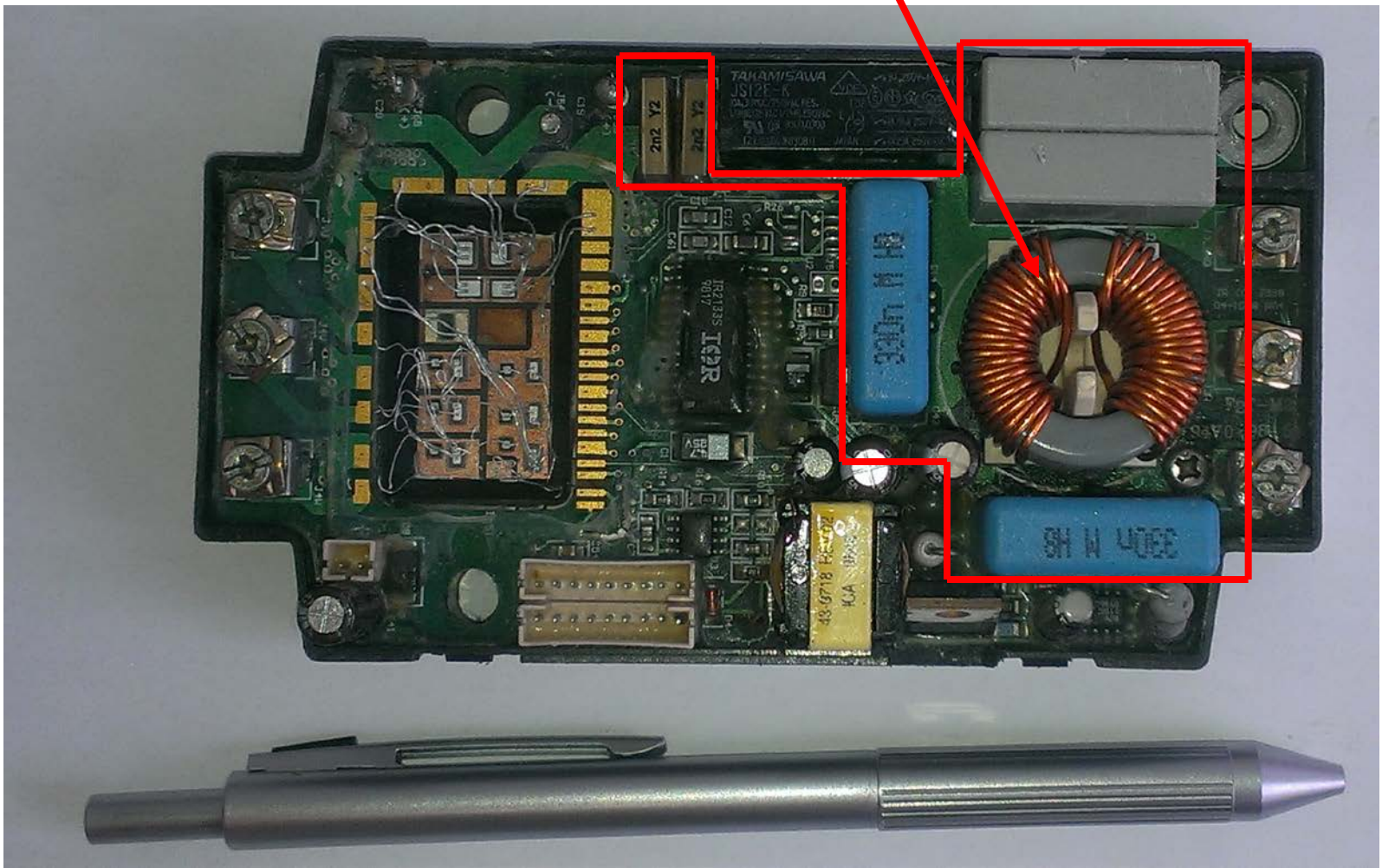
Relative losses [%]

Failure rate [h<sup>-1</sup>]



# 1.- Introduction

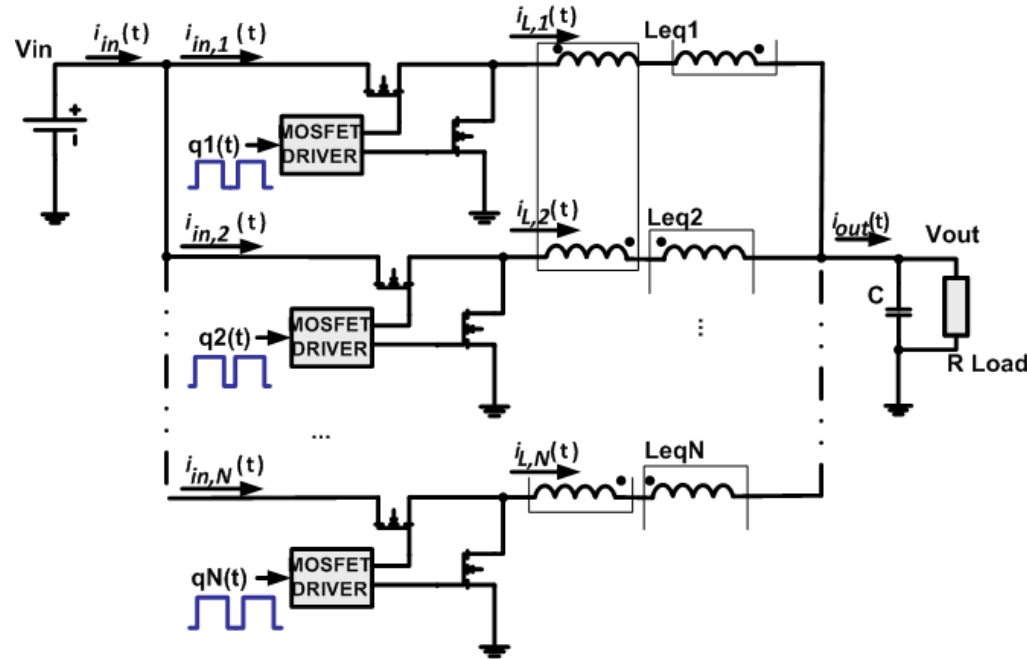
## EMI FILTER



# 1.- Introduction

- Switching Frequency Modulation (SFM) is a worthy way to suppress EMI in power converters
  - SFM applied to parallel arrangement should be combined with interleaving. This will result in Variable Delay Frequency Modulation (VDFM)
  - This technique is suitable for new devices (SiC)
- 
- Parallel arrangement is a disruptive topology that breaks frequency barrier. Moreover, Coupled Interleaved Multicellular Parallel Converters (CIMPC) show several advantages in terms of system integration and dynamic response
  - CIMPC require a **SYMETRIC** operation

## 2.- SFM in Parallel Arrangement

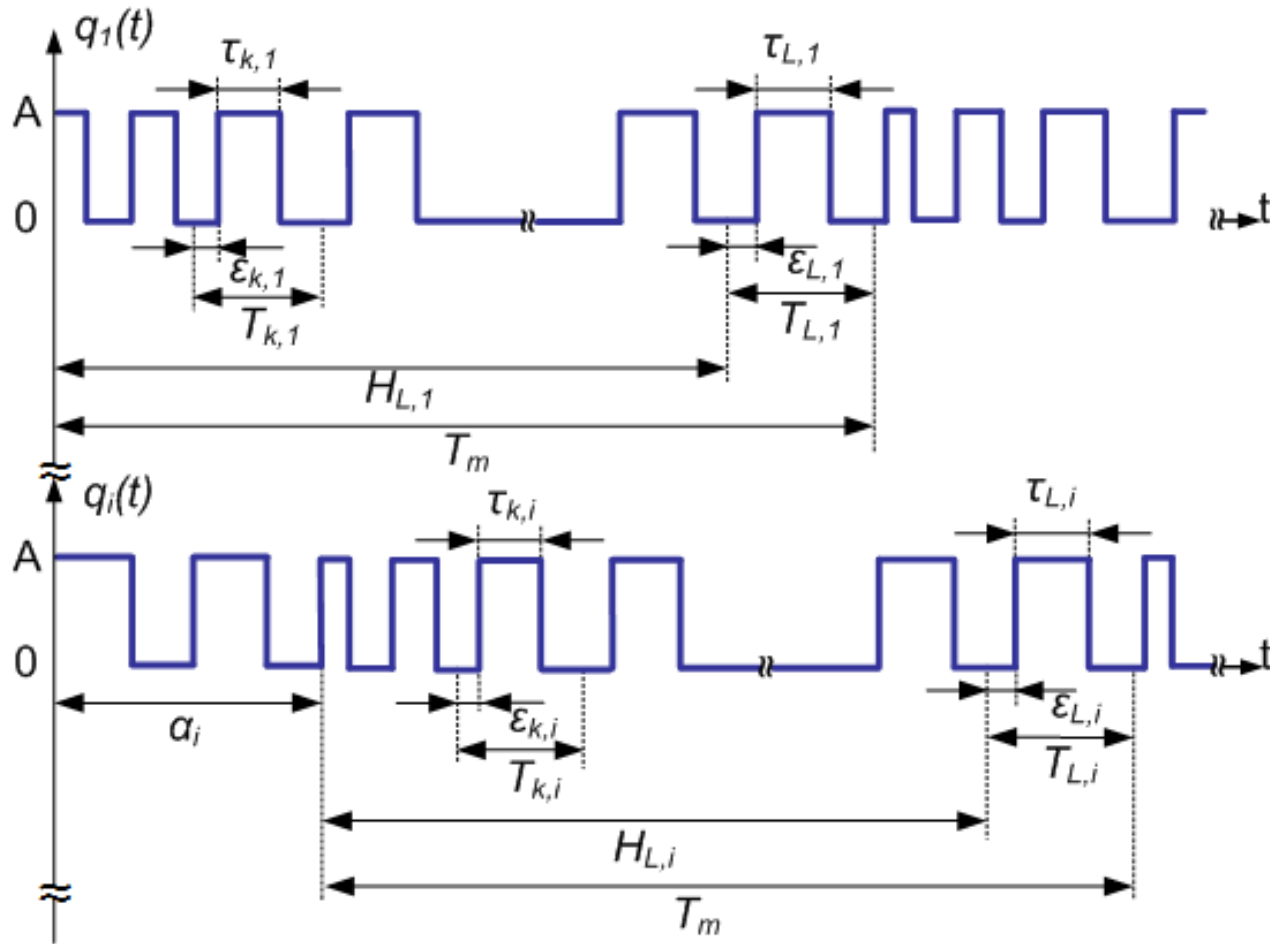


Breaks frequency barrier

Increased control dynamics

Redundancy without impairing reliability

## 2.- SFM in Parallel Arrangement



Periodic modulation function of period  $T_m$

## 2.- SFM in Parallel Arrangement

TABLE I  
CHARACTERISTICS OF DIFFERENT MODULATIONS

Modulations	$\varepsilon_{k,i}$	$T_{k,i}$	$\tau_{k,i}$	$\alpha_i$
CDFM-T <sub>m</sub>	$0 \quad \forall i,k$	$T_c + \Delta T_k \quad \forall i$	$D_c \cdot T_k \quad \forall i$	$\frac{T_m}{N}(i-1)$
CDFM-T <sub>c</sub>	$0 \quad \forall i,k$	$T_c + \Delta T_k \quad \forall i$	$D_c \cdot T_k \quad \forall i$	$\frac{T_c}{N}(i-1)$
VDFM	$\frac{T_{k,j}}{N}(i-1)$	$T_c + \Delta T_k \quad \forall i$	$D_c \cdot T_k \quad \forall i$	$0 \quad \forall i$

Periodic modulation function of period  $T_m$



## 3.- Variable Delay Frequency Modulation

### VDFM combines interleaving and SFM

$$\begin{aligned}
 S_{CDFM-T_m}(w) &= F\left\{\sum_{i=1}^N q_i(t)\right\} = NAD_c \partial(w) + \sum_{n=1}^{\infty} \left[ \frac{A}{j\pi n} \left( \frac{1 - e^{-j2\pi n}}{1 - e^{-j2\pi n/N}} \right) \sum_{k=1}^L \left[ e^{\frac{-j2\pi n H_k}{T_m}} \left( 1 - e^{\frac{-j2\pi n \tau_k}{T_m}} \right) \right] \partial(w - nw_m) \right] = \\
 &= NAD_c \partial(w) + N \cdot E_{CDFM-T_m}(w) \sum_{n=1}^{\infty} \left[ \frac{A}{j\pi n} \sum_{k=1}^L \left[ e^{\frac{-j2\pi n H_k}{T_m}} \left( 1 - e^{\frac{-j2\pi n \tau_k}{T_m}} \right) \right] \partial(w - nw_m) \right],
 \end{aligned}$$

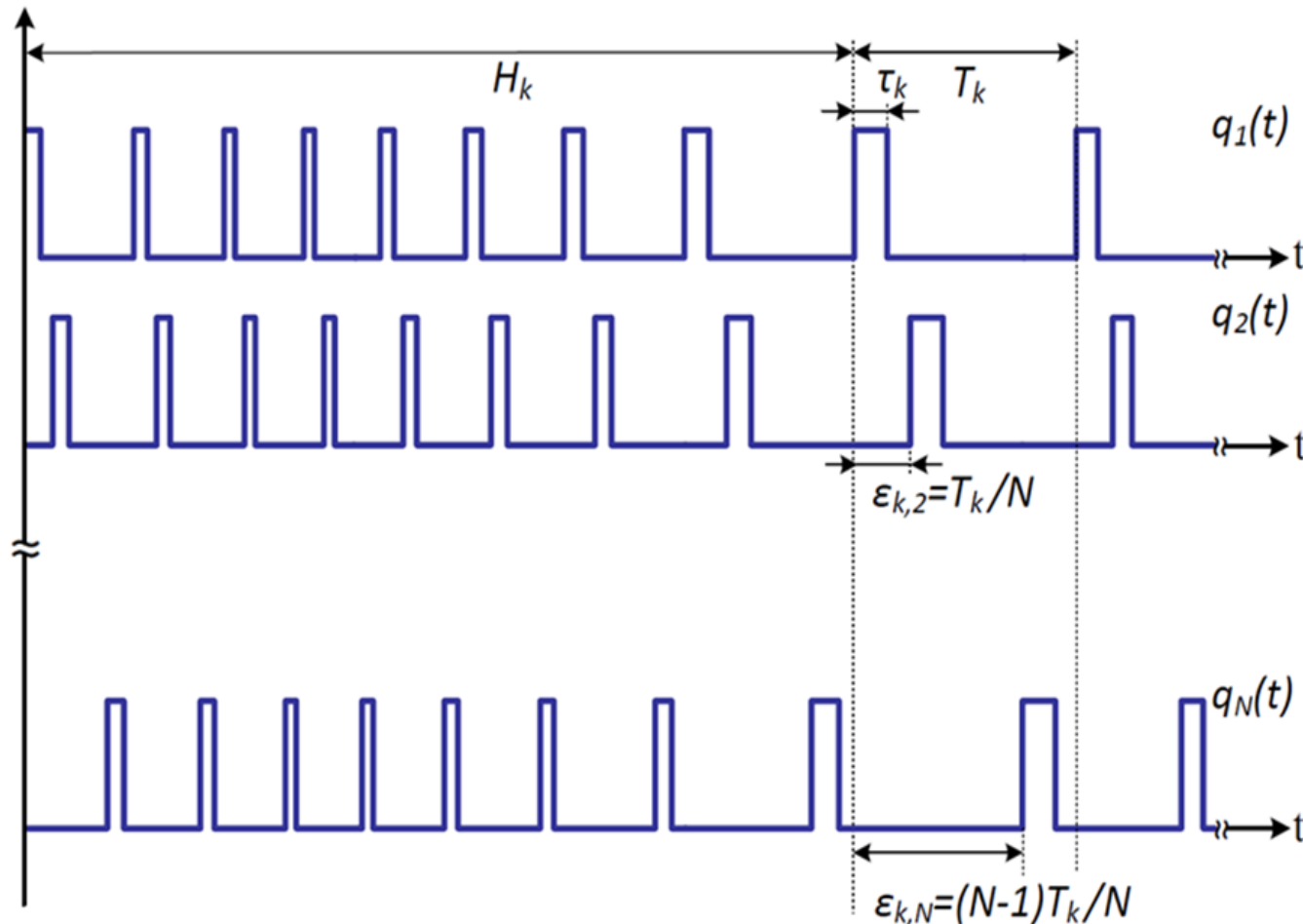
$$\begin{aligned}
 S_{CDFM-T_c}(w) &= F\left\{\sum_{i=1}^N q_i(t)\right\} = NAD_c \partial(w) + \sum_{n=1}^{\infty} \left[ \frac{A}{j\pi n} \left( \frac{1 - e^{\frac{j2\pi n}{L}}}{1 - e^{\frac{j2\pi n}{NL}}} \right) \sum_{k=1}^L \left[ e^{\frac{-j2\pi n H_k}{T_m}} \left( 1 - e^{\frac{-j2\pi n \tau_k}{T_m}} \right) \right] \partial(w - nw_m) \right] = \\
 &= NAD_c \partial(w) + N \cdot E_{CDFM-T_c}(w) \sum_{n=1}^{\infty} \left[ \frac{A}{j\pi n} \sum_{k=1}^L \left[ e^{\frac{-j2\pi n H_k}{T_m}} \left( 1 - e^{\frac{-j2\pi n \tau_k}{T_m}} \right) \right] \partial(w - nw_m) \right]
 \end{aligned}$$

$$S_{VDFM}(w) = F\left\{\sum_{i=1}^N q_i(t)\right\} = NAD_c \partial(w) + \sum_{n=1}^{\infty} \left[ \frac{A}{j\pi n} \sum_{k=1}^L \left[ \left( \frac{1 - e^{\frac{j2\pi n T_k}{T_m}}}{1 - e^{\frac{j2\pi n T_k}{NT_m}}} \right) e^{\frac{-j2\pi n H_k}{T_m}} \left( 1 - e^{\frac{j2\pi n \tau_k}{T_m}} \right) \right] \partial(w - nw_m) \right]$$

$\alpha_i=0$  ;  $\tau_k$  control ;  $T_k$  modulated,  $\varepsilon_k=(i-1)T_k/N$

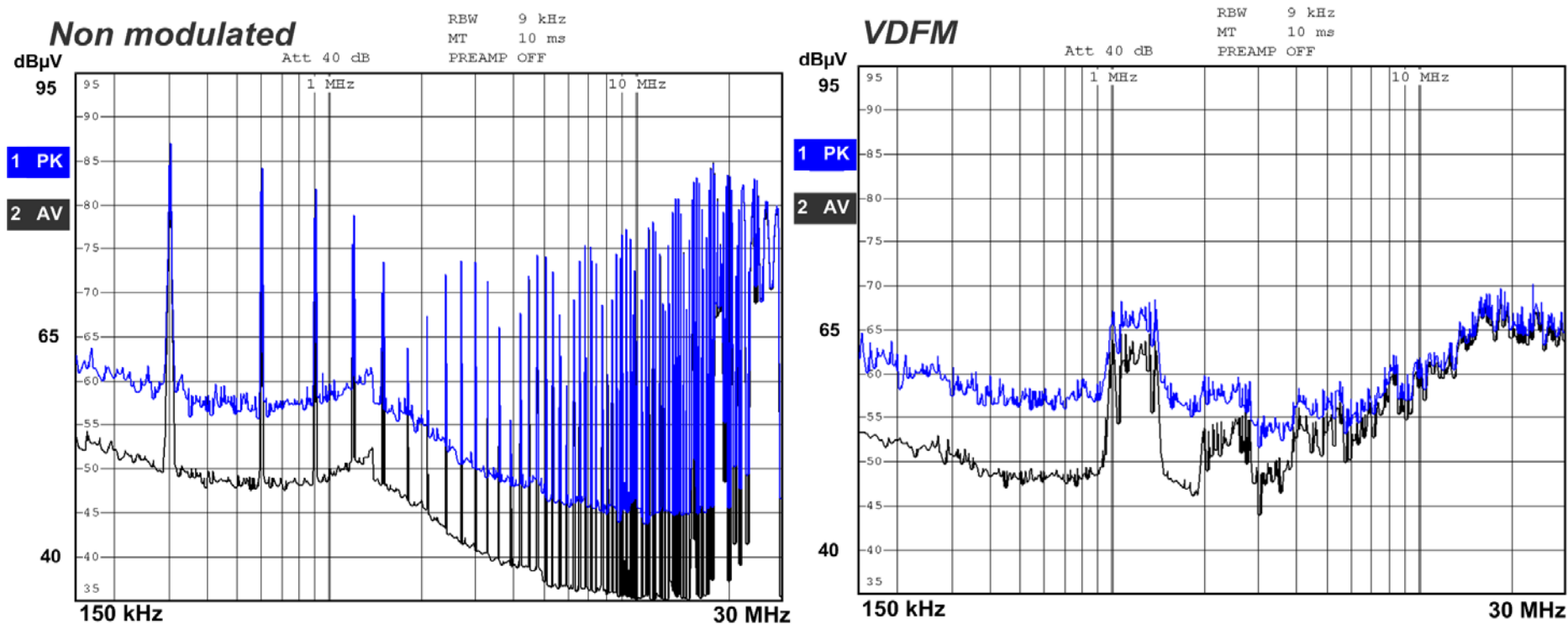
### 3.- Variable Delay Frequency Modulation

**VDFM combines interleaving and SFM**



$\alpha_i=0$  ;  $\tau_k$  control ;  $T_k$  modulated,  $\epsilon_k=(i-1)T_k/N$

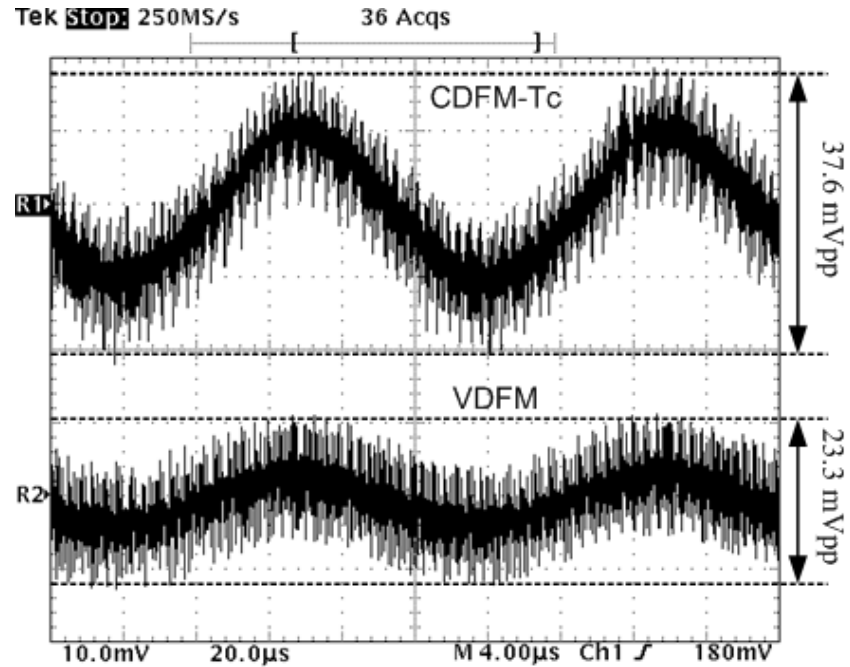
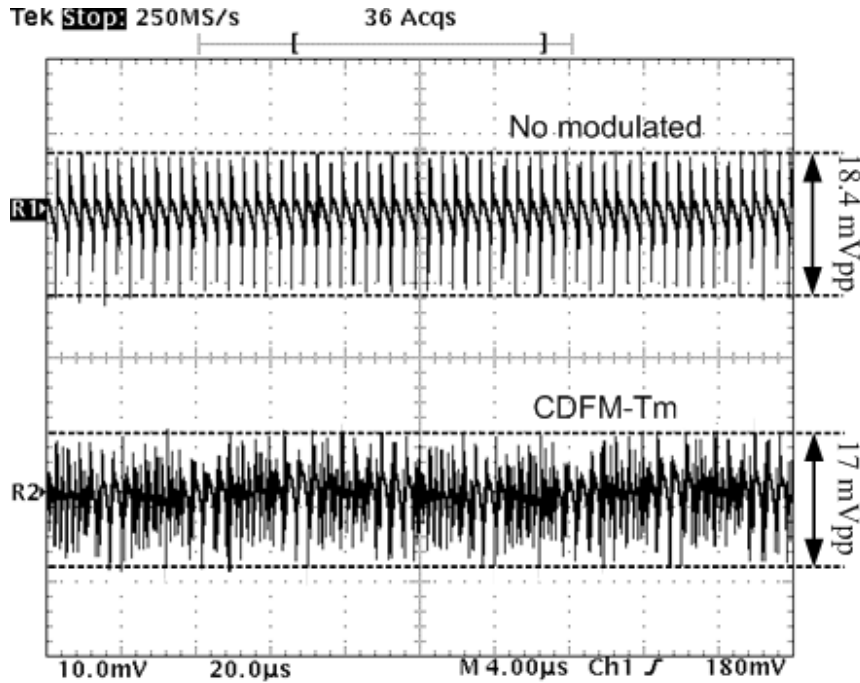
# 3.- Variable Delay Frequency Modulation



*Example of VDFM performance:*

$$N=4 ; f_c=300\text{kHz} ; m=6$$

# 3.- Variable Delay Frequency Modulation

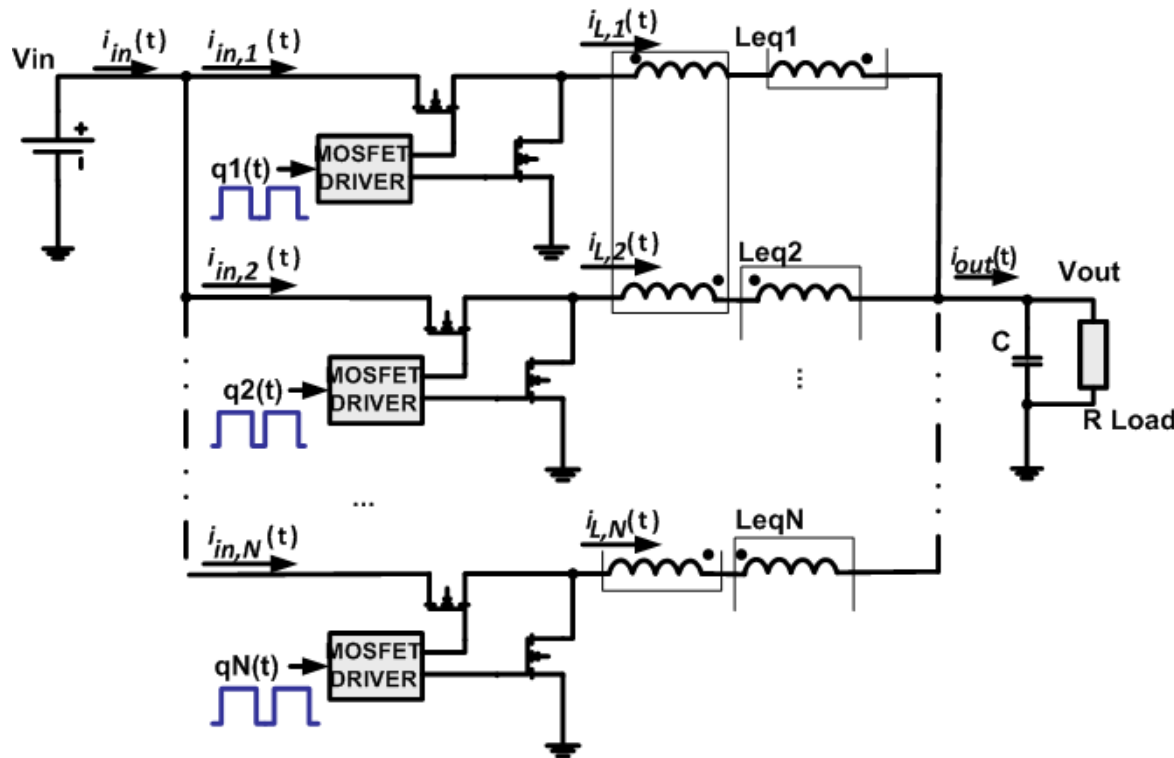


*Example of VDFM performance:*

$$N=4 ; f_c=300\text{kHz} ; m=6$$

# 4.- Coupled Interleaved Multicellular Parallel Converter

We need a **SYMETRIC** system in order to prevent couplers saturation, that could lead to a catastrophic failure.



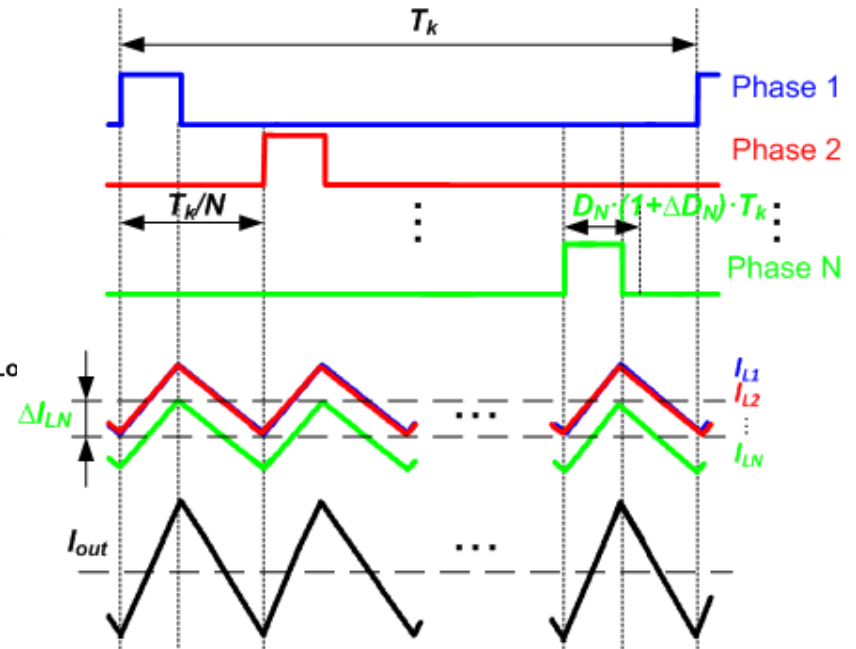
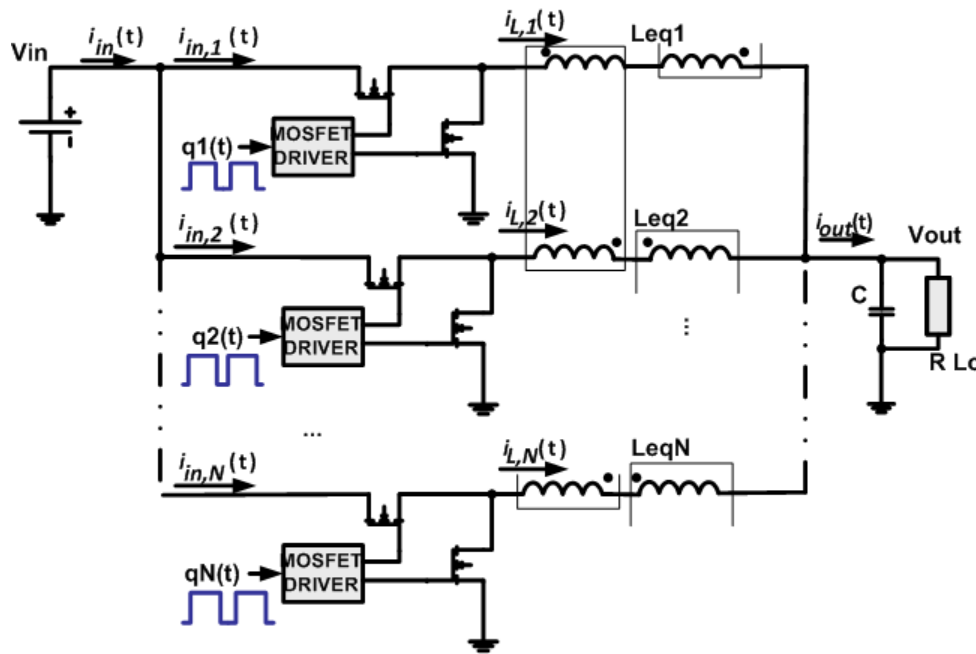
- SYMETRIC**
- Construction**
- Gates drive**
- Switching**

# 4.- Coupled Interleaved Multicellular Parallel Converter

Duty-cycle

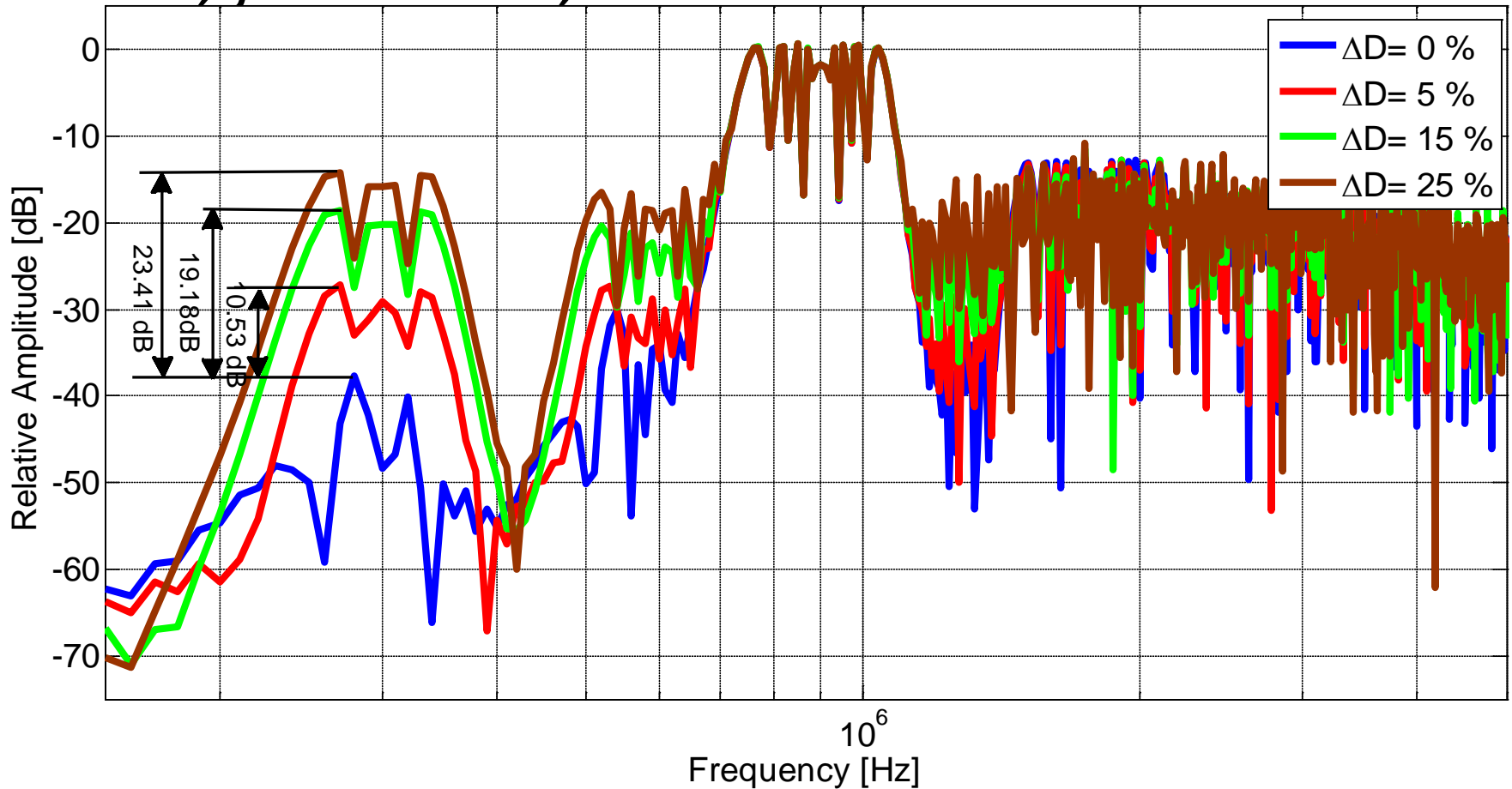
For phase  $N$

$$D_N = D_c \cdot (1 + \Delta D)$$



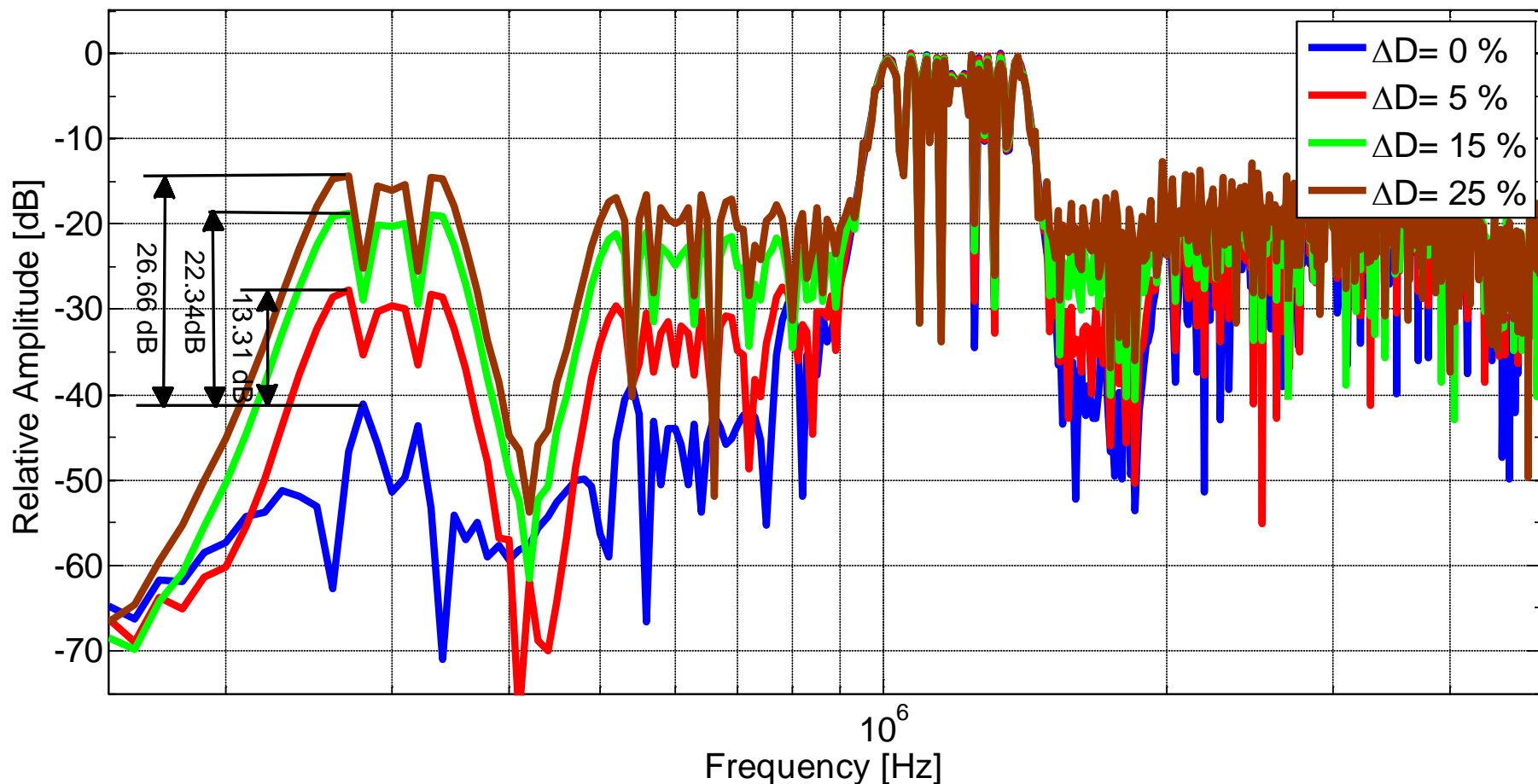
# 4.- Coupled Interleaved Multicellular Parallel Converter

$N=3 ; f_c=300\text{kHz} ; m=6$



# 4.- Coupled Interleaved Multicellular Parallel Converter

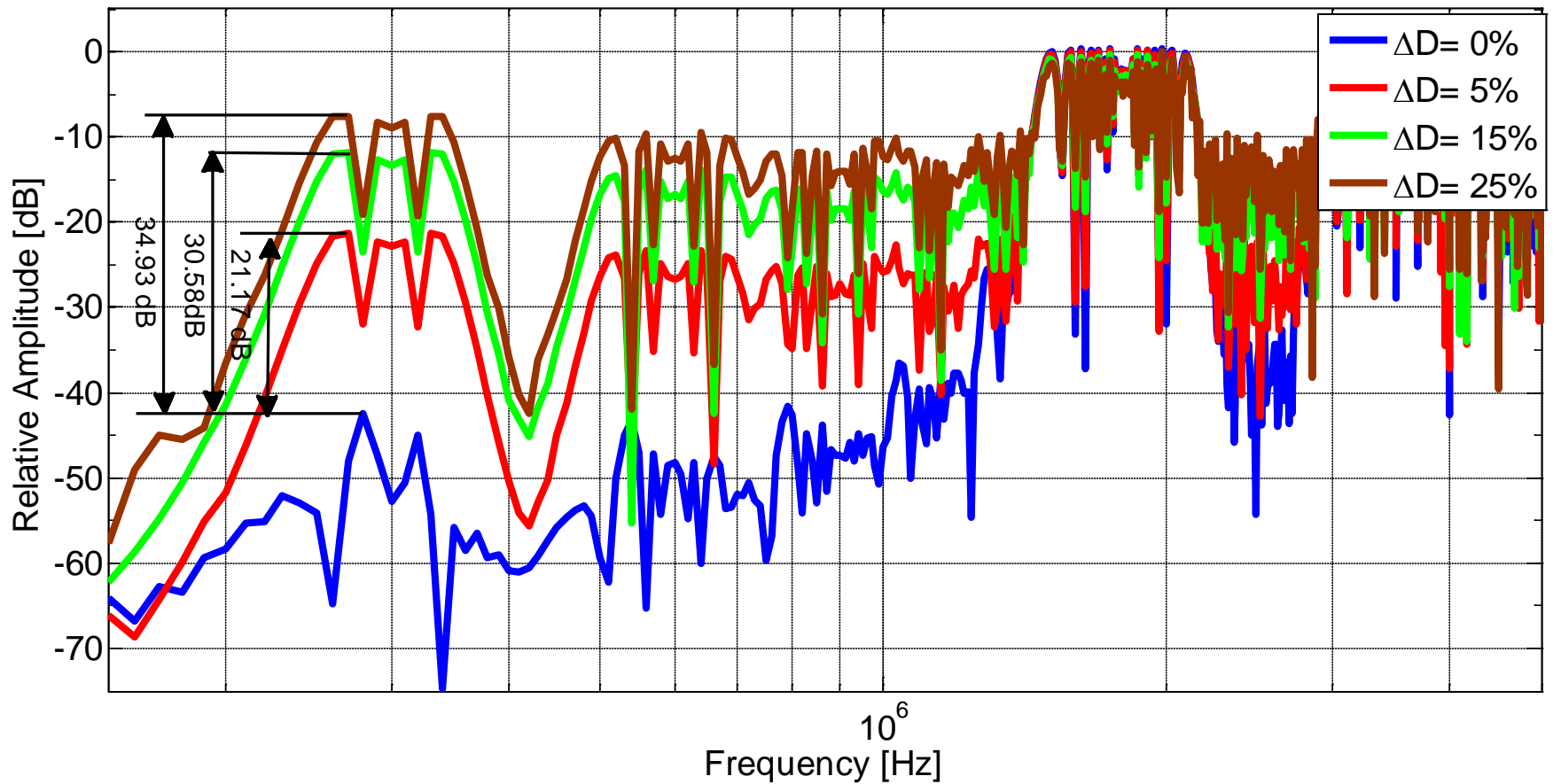
$N=4 ; f_c=300\text{kHz} ; m=6$



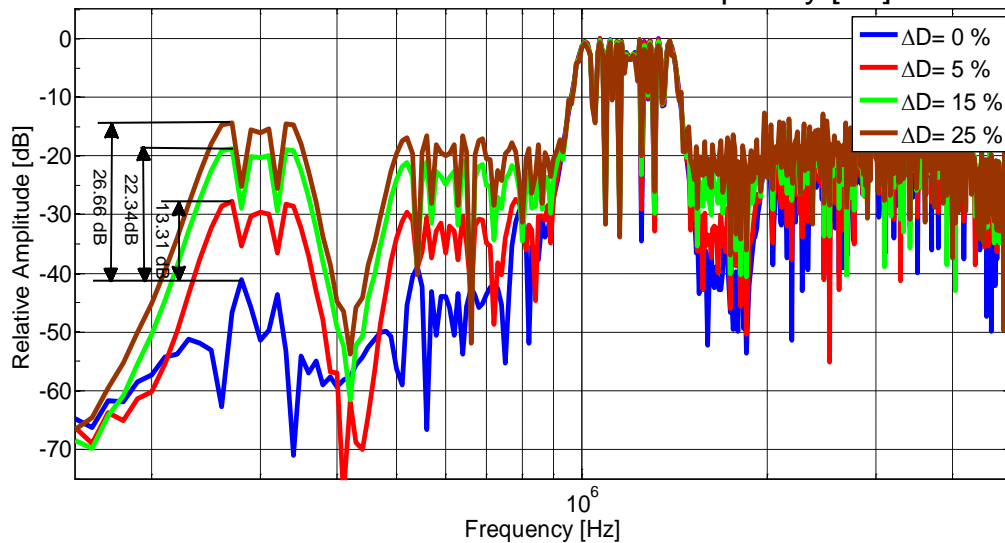
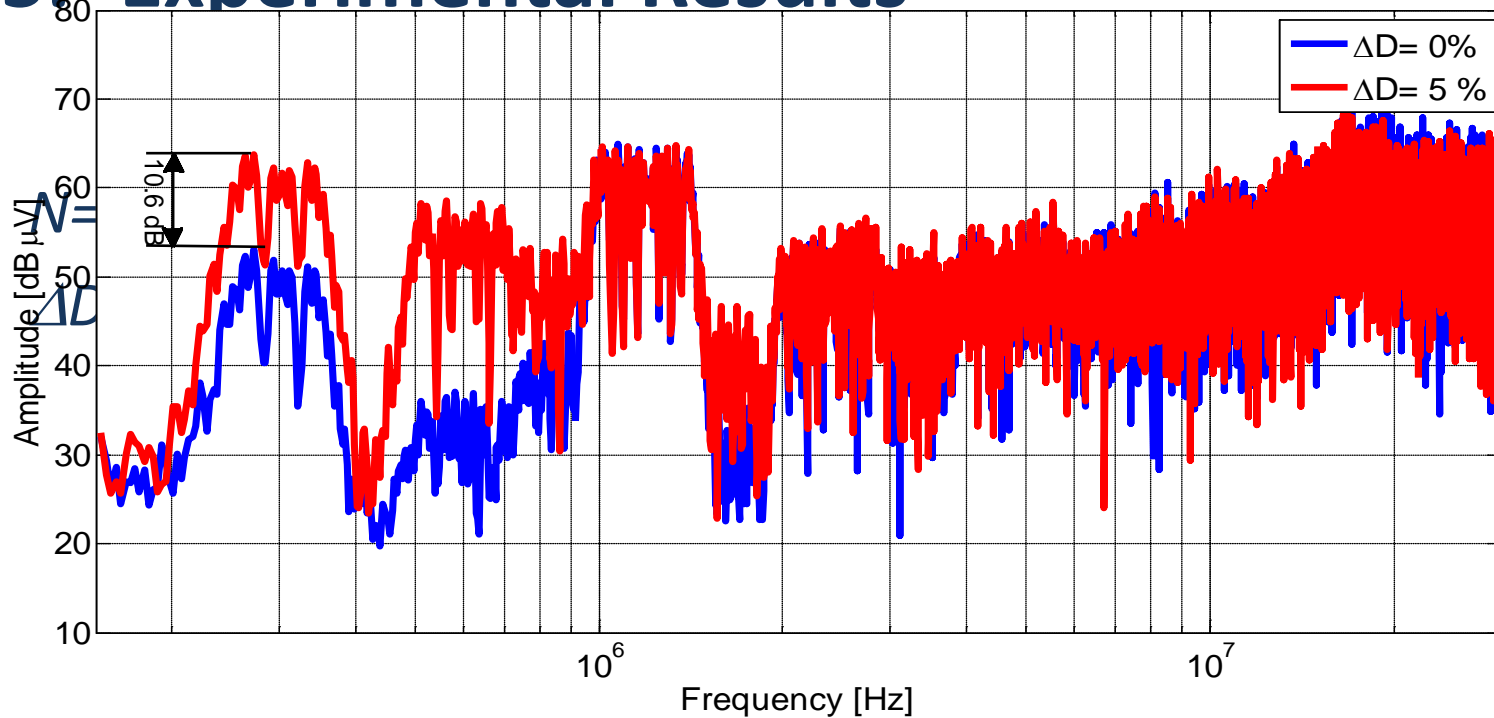


# 4.- Coupled Interleaved Multicellular Parallel Converter

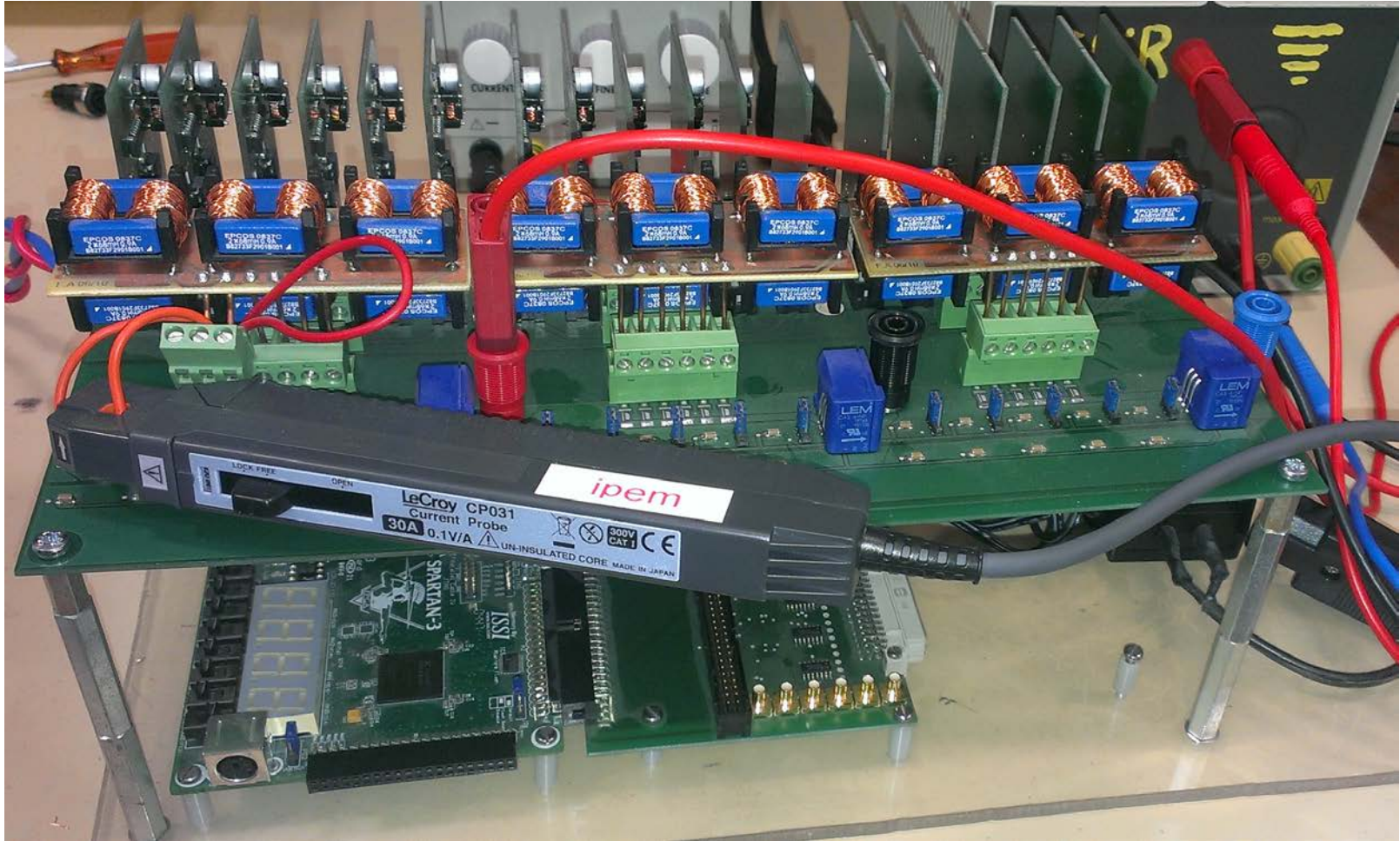
$N=6 ; f_c=300\text{kHz} ; m=6$



# 5.- Experimental Results

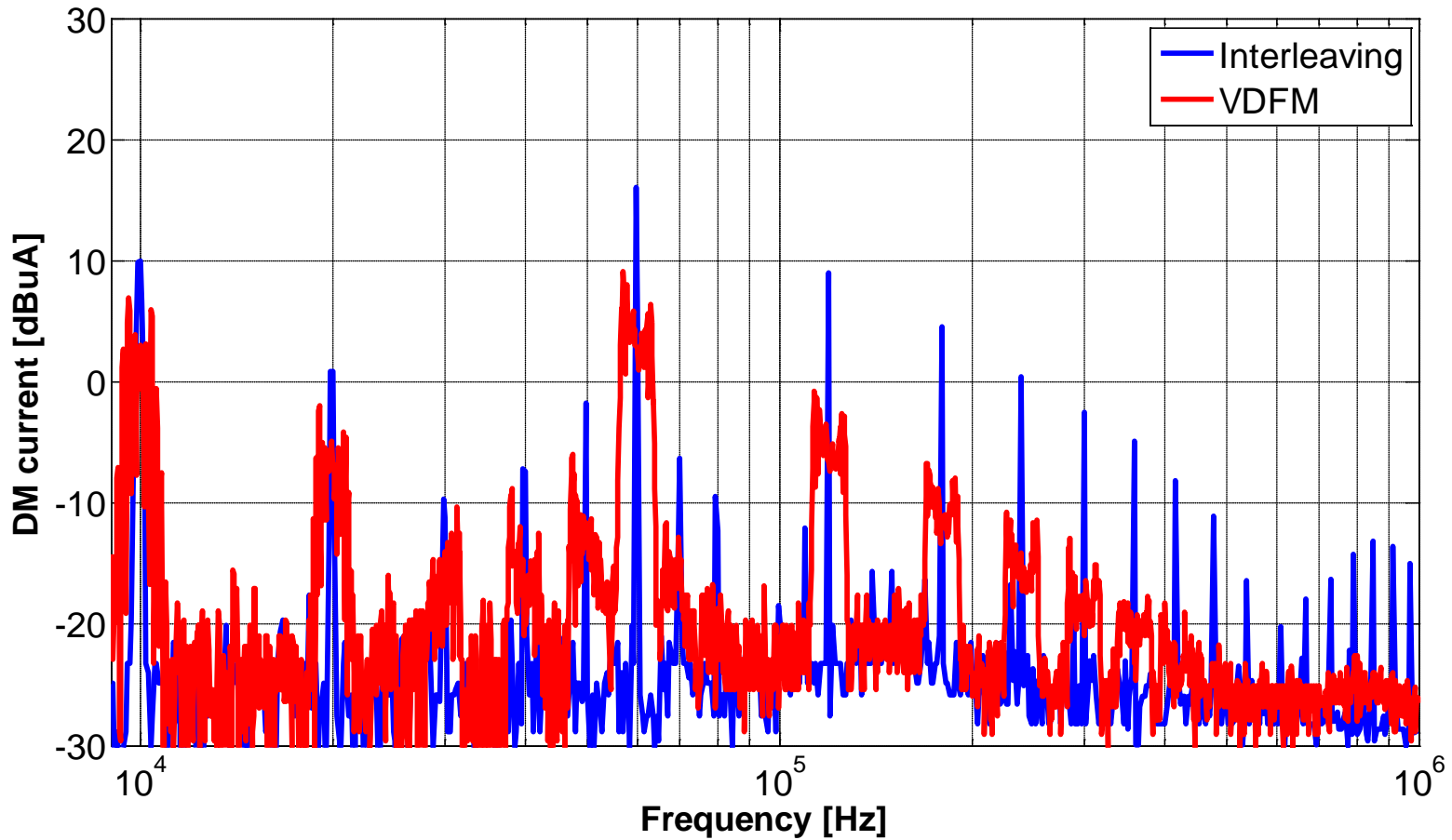


# 5.- Experimental Results



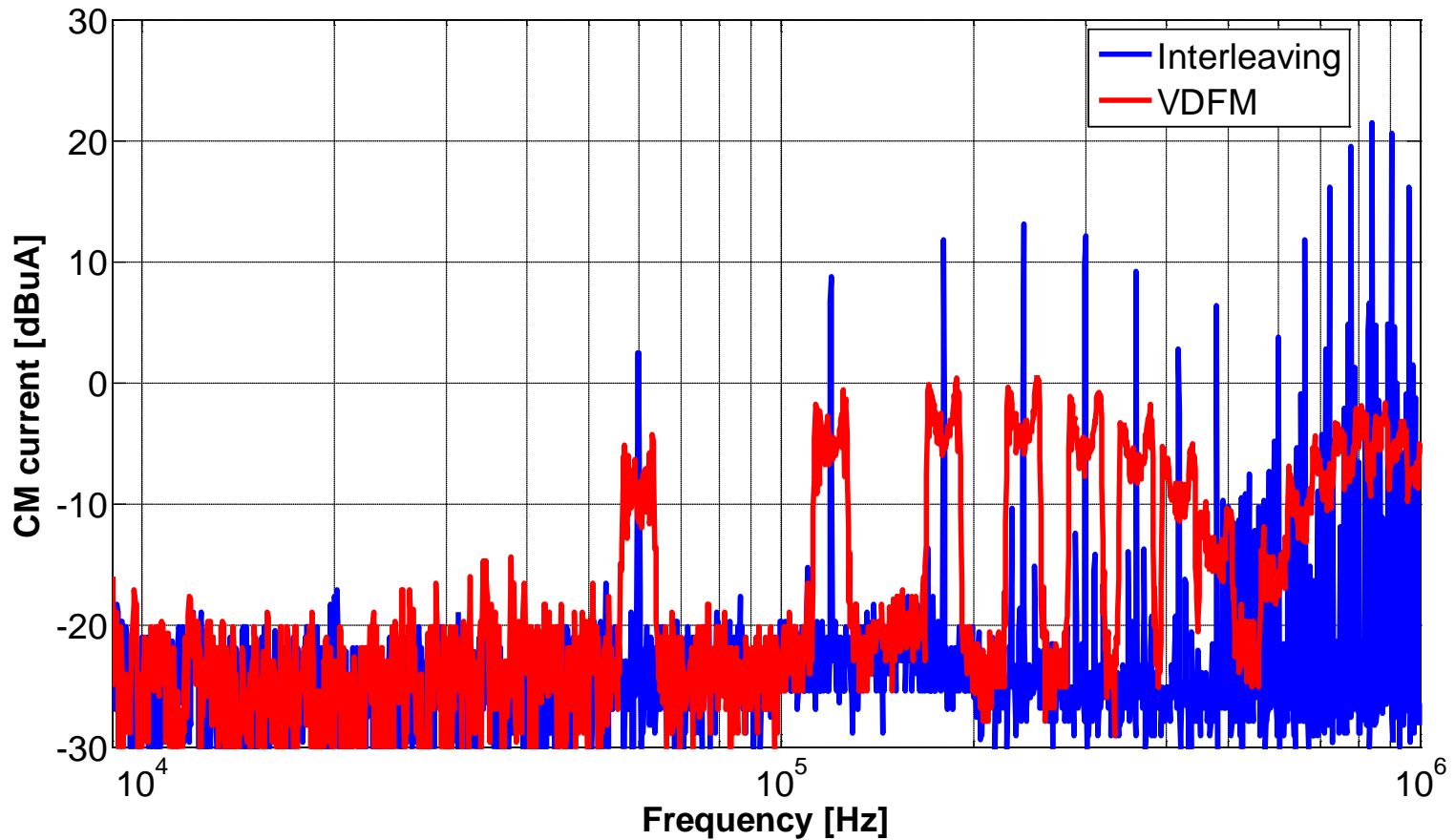
*CIMPC N=6 ; DC/DC ;  $V_{in}$ = 311V ;  $V_{out}$ = 48V ;  $P_o$ =250W*

# 5.- Experimental Results



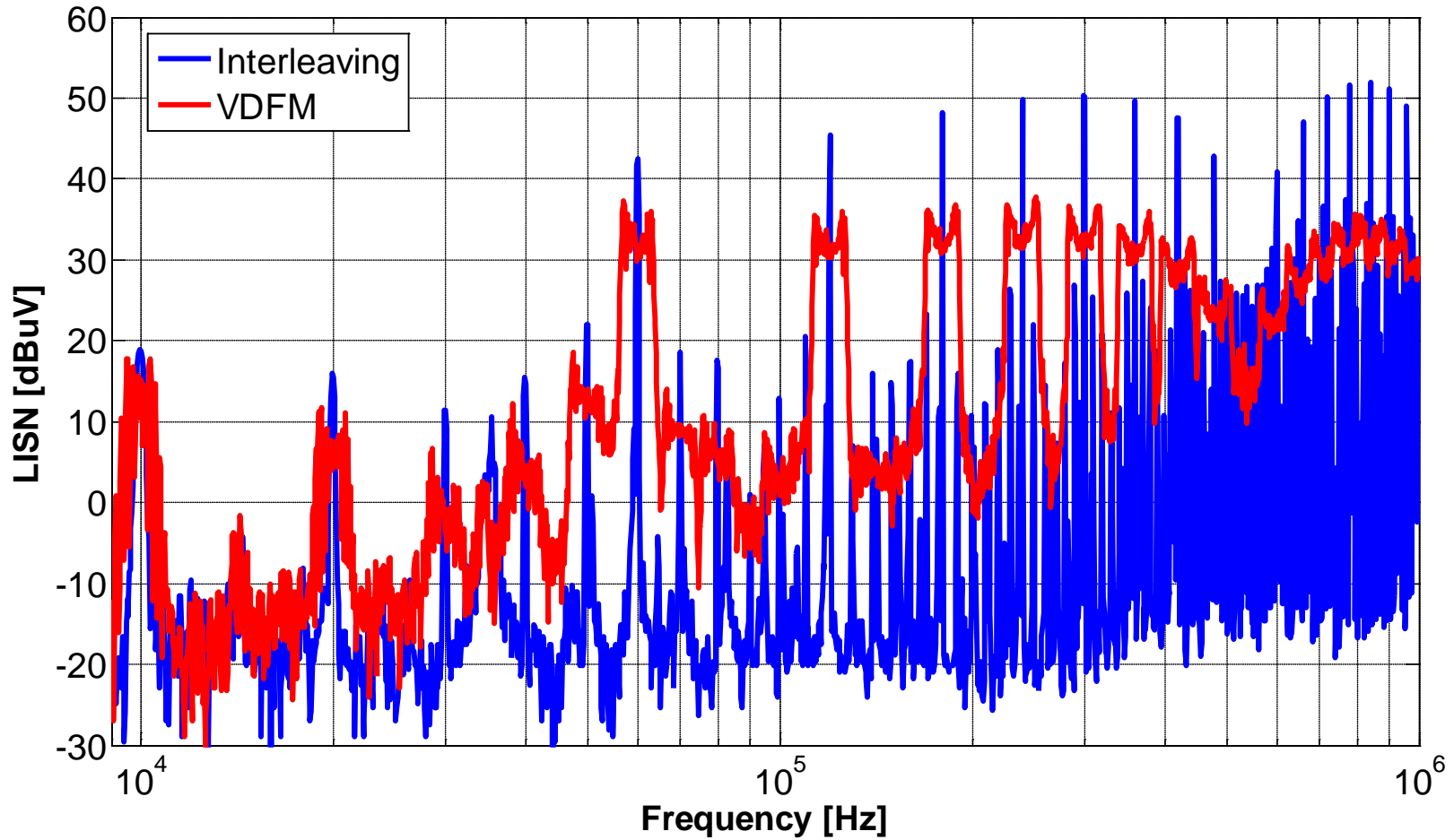
*N=6 ; f<sub>c</sub>=10kHz ; m=6*

# 5.- Experimental Results



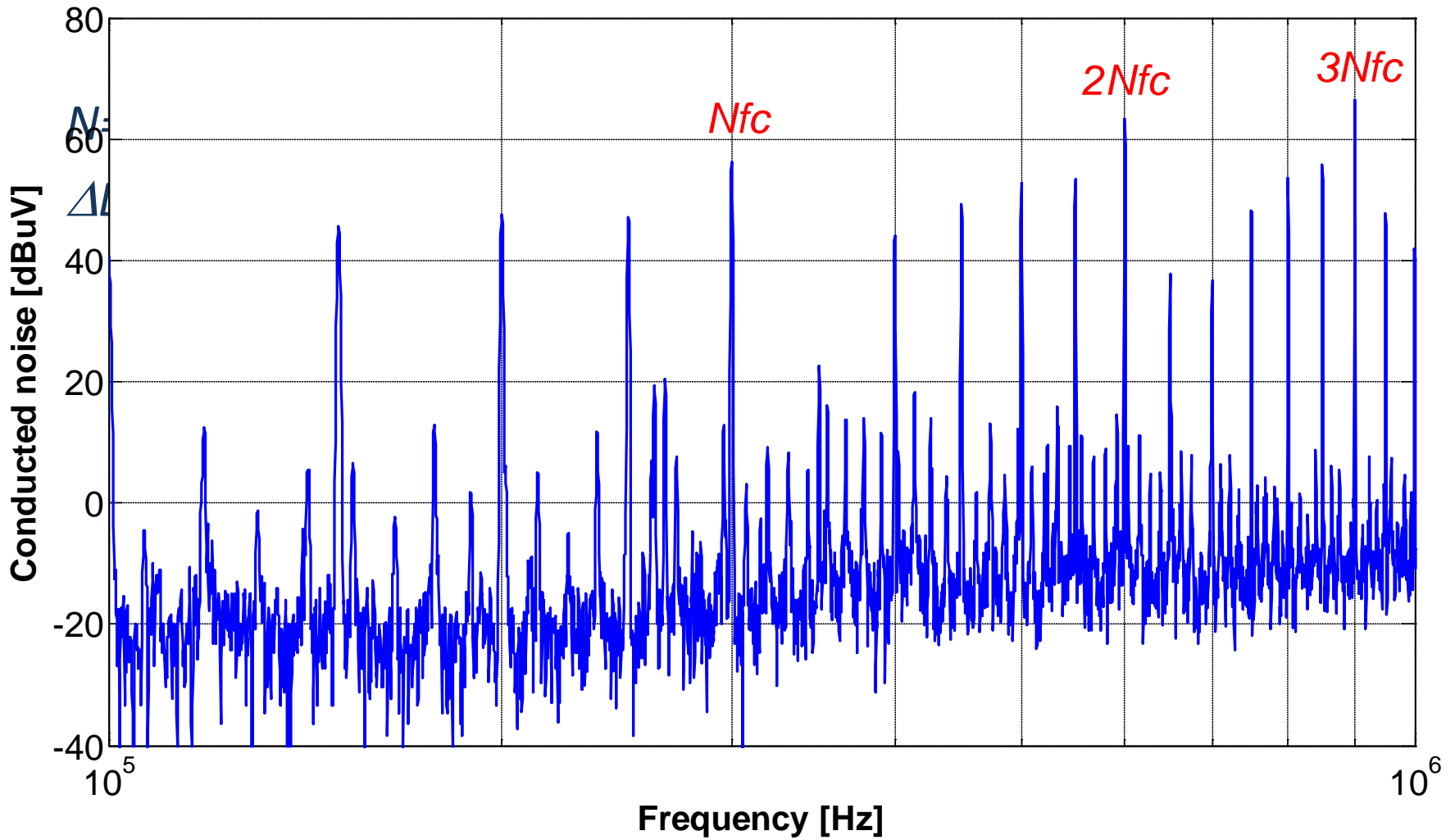
$N=6 ; f_c=10\text{kHz} ; m=6$

# 5.- Experimental Results



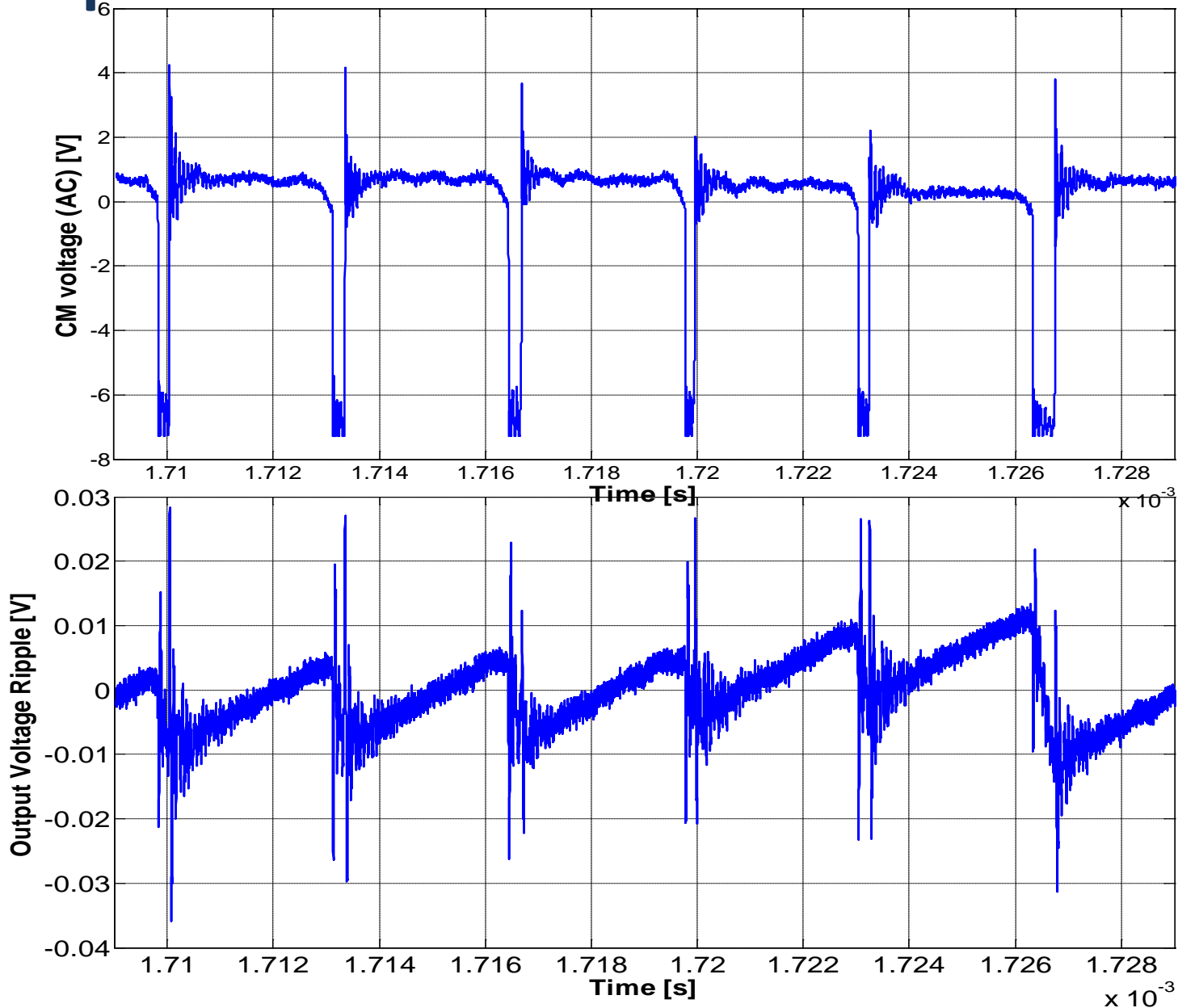
$N=6 ; f_c=10\text{kHz} ; m=6$

# 5.- Experimental Results



$N=6 ; f_c=50\text{kHz} ; m=6$

# 5.- Experimental Results





## 5.- Conclusions

*-VDFM could be applied successfully to CIMPC to suppress conducted noise*

*-New Devices (SiC, GaN) are candidates to use this technique*

*-Duty-cycle deviations ( $\Delta D$ ) produce the following effects:*

- None at  $N_{fc}$*
- Attenuation degradation is noticed below  $N_{fc}$*
- Attenuation degradation increases with  $N$*

*- Precise timing in gate-drive signals is a keypoint for this particular application*